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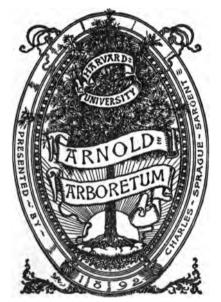
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# UNITED STATES DEPARTMENT OF AGRICULTURE BULLETIN No. 676

Contribution from the Forest Service HENRY S. GRAVES, Forester

FOREST PRODUCTS LABORATORY, Madison, Wisconsin In Cooperation with the University of Wisconsin

Washington, D. C.

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PROFESSIONAL PAPER

July 16, 1919



## THE RELATION OF THE SHRINKAGE AND STRENGTH PROPERTIES OF WOOD TO ITS SPECIFIC GRAVITY

By

J. A. NEWLIN, in Charge, Section of Timber Mechanics, and T. R. C. WILSON, Engineer in Forest Products

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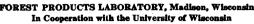
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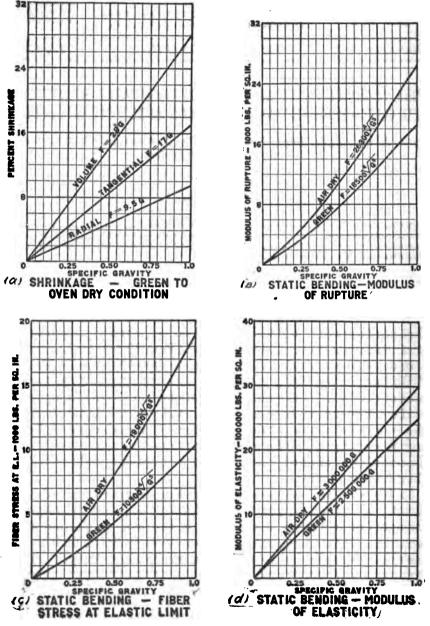
#### PURPOSE.

It has long been recognized that there are direct relations between the specific gravity, or density, of a wood and its strength properties.¹ By the analysis of over 200,000 tests, the Forest Products Laboratory, conducted in cooperation with the University of Wisconsin, Madison, Wis., has now definitely established these relations. It is the purpose of this bulletin to state these relations and to put the expression of them in such form as to render them easily useful (1) for estimating the properties of any particular timber; (2) for selecting timber for any given purpose; (3) for comparing the various species; and (4) for determining in what way the species are exceptional and to what uses they are best adapted.

It has usually been assumed that the strength of wood varies directly with the first power of its density; i.e., that the respective strengths of two sticks would differ in the same proportion as the densities. It was recognized that fiber stress at elastic limit in compression perpendicular to the grain, or bearing strength on side

Accurate determinations made at the Forest Products Laboratory on seven species of wood, including both hardwood and confierous species, showed a range of only about 4½ per cent in the density of the wood substance, or material of which the cell walls are composed. Since the density of wood substance is so nearly constant, it may be said that the density or specific gravity of a given piece of wood is a measure of the amount of wood substance contained in it.

surface, and work values in static bending or toughness, deviate very erratically from this relation; but the relation was supposed to hold especially true in the case of such properties as modulus of rupture, or maximum bending strength, and strength in compression parallel



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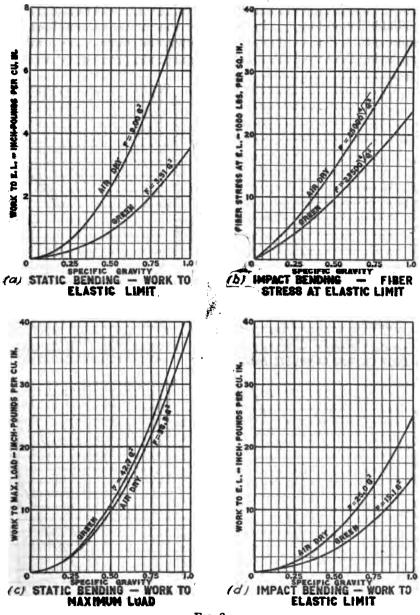


Fig. 2.

to the grain, or strength as a column. It has also been supposed that the relation applied between pieces of the same species, between pieces of different species, and between average results of strength tests on different species. A study of the data at present available, which are derived from a much larger number of tests and which cover a greater

range in specific gravity and strength values than was true of the data available heretofore, made it evident that these assumptions were inaccurate and that there was a better and more correct method expressing the actual relations between specific gravity and strength.

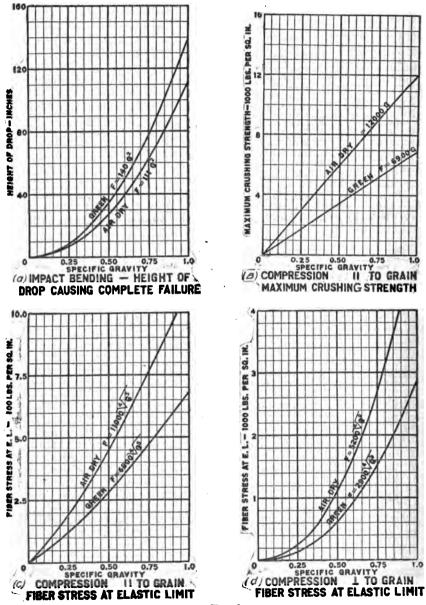


Fig. 3.

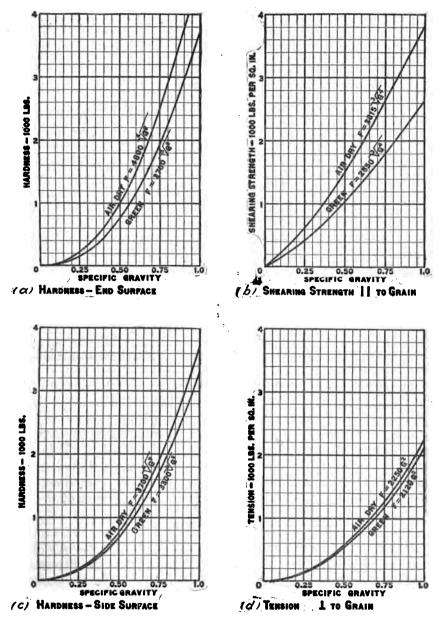


Fig. 4.

In order that the relation between specific gravity and each of the various mechanical properties of wood may be easily put to practical use, the relation, both for green and for air-dry material, is given in the form of an equation (Table 1) and, in addition, in the form of a curve (figs. 1 to 4).

### SPECIES-LOCALITY AVERAGES.

The specific-gravity relations given in this bulletin are derived from a study of what may be called "species-locality" averages; that is, each average represents tests of material of one species from one locality.

There are two principal reasons for using "species-locality" averages in preference to the results of individual tests. First, the number of individual tests is quite large, amounting in some instances to as many as 900 from a single "species-locality", so that an immense amount of work is saved by the use of the "species-locality" averages; second, if individual tests were used, the "species-localities" having larger trees or a larger number of trees would include a larger number of tests and would have undue weight in determining the relations.

The method of analysis used is applicable also to individual tests from a single species to determine the specific gravity relations within that species. It has been applied to a few of the properties of some of the more important species which are used for structural timbers where there was a rather large number of test pieces and a considerable range in specific gravity.

### DETERMINATION OF SPECIFIC GRAVITY.

Specific gravity of wood, as used herein, is based on the volume of the specimens when tested (green or air-dry) and their weight when in an oven-dry condition; that is, it is the ratio of the weight of the specimen of wood, oven-dry, to the weight of a volume of water equal to the volume of the specimen at the time of test. Because of the shrinkage which takes place in wood when it is dried, this figure is not the true specific gravity of a piece of oven-dry wood. The method, however, is easily applied to each specimen tested, and is the standard method of the Forest Service for the determination of a specific-gravity figure for use in studying the properties of wood.

### MOISTURE CONTENT OF TEST SPECIMENS.

Both green and air-dry specimens were used in the tests, and the relations between specific gravity and strength were determined separately for green and air-dry wood. Variations in the moisture content of wood have no effect on its mechanical properties so long as the wood is thoroughly green; they have considerable influence on these properties, however, as soon as the wood becomes air-dry, or partially air-dry. Accurate comparisons can not be made between the properties of two lots of air-dry specimens unless they were tested at the same moisture content or adjustments made in the strength figures for difference in moisture content.

The moisture content of the air-dry material at the time of test varied from 8 to 18 per cent. Modulus of rupture and maximum strength in compression parallel to the grain were adjusted to a moisture content of 12 per cent before determinations of the relation of these properties to the specific gravity was made. This adjustment was possible because the laws governing the variation of these properties with varying moisture content are fairly well established. However, in the case of the other strength functions their variation with varying moisture content has not been studied in detail and no such adjustment is possible with any very great degree of accuracy. Consequently, the actual moisture content values as obtained from tests have been used in the determination of the relation of these properties to specific gravity.

### THE EQUATIONS.

Table 1 and figures 1 to 4 give equations which represent the average relations between specific gravity and each of the mechanical properties. All the "species-locality" averages available on any particular property were considered in deriving the equations for that property. The number of "species-locality" averages from which an equation is derived varies from 84 to 178. This variation is due to the fact that several of the tests were not used in some of the earlier testing work and to the fact that tests have not yet been completed on air-dry material for all of the "species-localities" listed.

Table 1 gives first the equations for shrinkage and for each of the strength properties of green and air-dry wood in terms of the specific gravity. These equations, as explained in the appendix, are reduced to a simple form; and the powers of gravity used are such that the equations may be solved by arithmetical operations and without the use of higher mathematics. However, to simplify even further the use of the equations, figures 1 to 4 have been prepared for their solu-Each of the curves shown in these diagrams represents the equation connecting specific gravity and one of the properties of The curves representing the equations for radial, tangential. and volumetric shrinkage appear in figure 1(a). In each of the other figures, 1(b) to 4(d), appear two curves for some one mechanical property. One of these curves is for green and the other for air-dry material. If the specific gravity is known, the equation value for any one or all of the properties of the wood in question may be readily determined from the curves without computation.

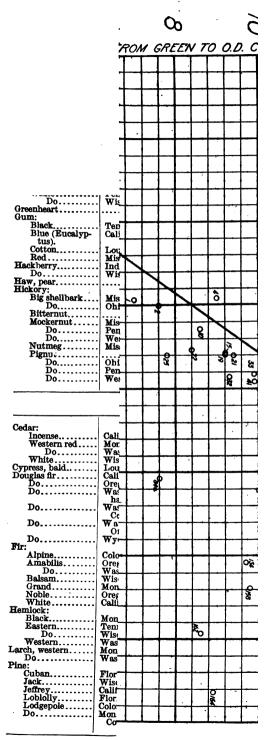
The second portion of Table 1 gives what may be termed a measure of the accuracy of the respective equations. It is not to be expected that all the "species-locality" averages will satisfy the equation exactly or even very closely. Some of the properties are more erratic than others, so that one "species-locality" may far exceed

the equation values and another "species-locality" fall far below them.

In figure 5 are plotted the curves of the equation for modulus of rupture in static bending in green material,  $M=18500\sqrt[4]{g^5}$ , and of the equation for the same property in air-dry material,  $M=26200\sqrt[4]{g^5}$ . In order to give a graphical idea as to the reliability of these equations, the specific gravity and the modulus of rupture of each "species-locality" have been plotted as a point. The reference number placed near each plotted point is assigned to the "species-locality" in the order of its respective specific gravity as determined from compression parallel to grain specimens of green wood. In figures 6, 7, and 8 the data are given for the curves on shrinkage in volume from green to oven-dry condition, maximum crushing strength in compression parallel to grain, and fiber strength at elastic limit in compression perpendicular to grain.

Under each property is listed in this second portion of Table 1, for both green and air-dry conditions, those percentages of the equation value above which were one-tenth of the "species-localities." Similarly, there are listed those percentages above which were one-fourth of the "species-localities," those below which were one-fourth, and those below which were one-tenth. For instance, in static bending (green), one-tenth of the "species-localities" tested had a modulus of rupture of more than 114 per cent of what the specific gravity equation indicated they should have had; one-fourth of them had a modulus of rupture greater than 108 per cent of the equation value; one-fourth of them less than 91 per cent of the equation value; and the lowest one-tenth had a modulus of rupture less than 84 per cent of what the equation indicated they should have had. It follows from these figures that one-half of the "species-localities" had a modulus of rupture of between 91 per cent and 108 per cent of the value given by the equation, and that the other one-half were evenly divided between those that were more than 108 per cent and those that were less than 91 per cent.

The third portion of Table 1 gives the actual value of each property for each "species-locality" as determined by the tests, expressed as a percentage of the value computed from the specific gravity by the use of the equation at the head of the column. For instance, it is found from the table that air-dry Biltmore ash has a modulus of rupture 98 per cent as great as that of the average wood of its specific gravity, the modulus of rupture of the average wood of this specific gravity being the figure given by the equation. These percentages are given for both green and air-dry wood.



the equation valu them.

In figure 5 are rupture in static the equation for th In order to give equations, the spe "species-locality" ber placed near eac in the order of compression paral 6, 7, and 8 the da sconsin... 53 165 Parish. Willow.. Louisiana 109 109 122 105 164 35 Arkansas... Wisconsin... Yellow..... from green to ovinessee. 68 147 compression para lifornia. Indiana.. Osage orange..... Poplar, yellow (tulip Tennessee. 76 54 90 78 146 compression perpession tree). Rhododendron, great ...do..... 85 51 156 49 89 61 63 65 45 Sassafras..... Serviceberry..... Silverbell tree.... Under each prodensin... ...do..... ....do..... both green and aido..... ....do..... ...do.... Wisconsin. value above whick sissippi. 135 154 139 144 159 155 112 Indiana.... larly, there are lis do.... Do..... Umbrella, Fraser... Tennessee ....do..... of the "species-logistylvania those below whickerships whickerships those below whickerships whickerships with the second Willow: Black.... Western black... 11 43a 114 Wisconsin. Oregon..... 148 157 160 Witch hazel.... Tennessee. (green), one-tenthonomics rupture of more that Virginia... indicated they sho CONIFERS. rupture greater th Pine—Continue... Lodgepole..... of them less than fornia 26 Montana, Granite 419 one-tenth had a mitana..... 2 10 1 62 45a 67a 46a County. Montana, Jefferson Do..... 40a equation indicate consin.... County. Wyoming.... Florida.
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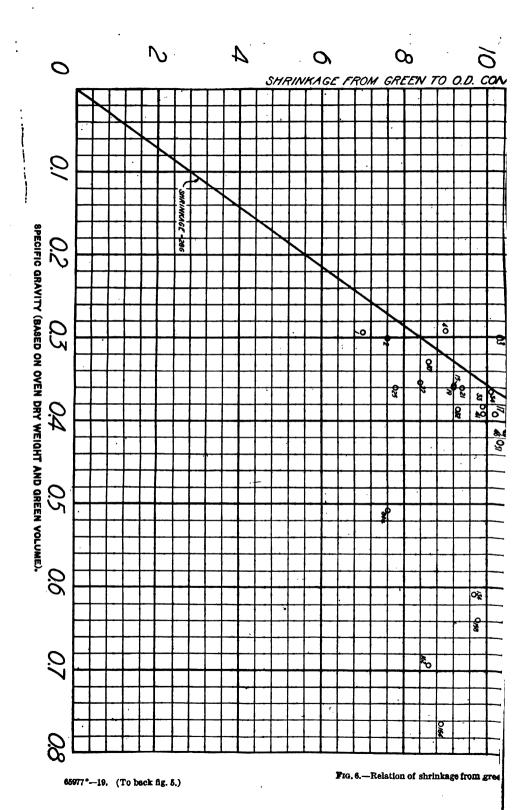
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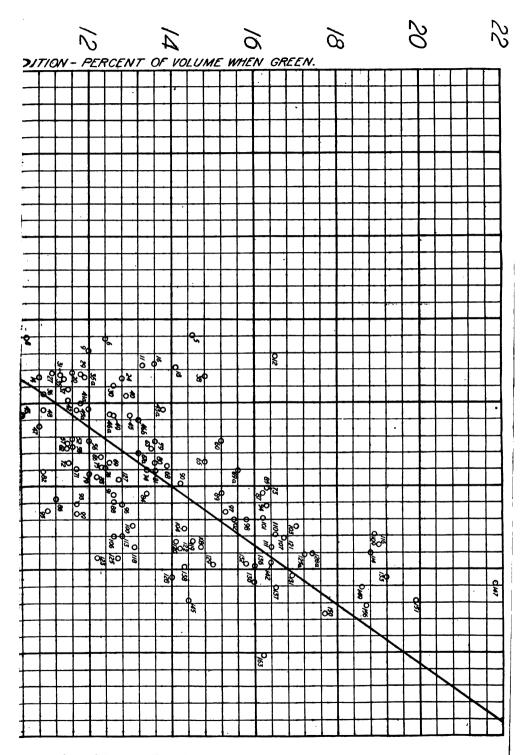
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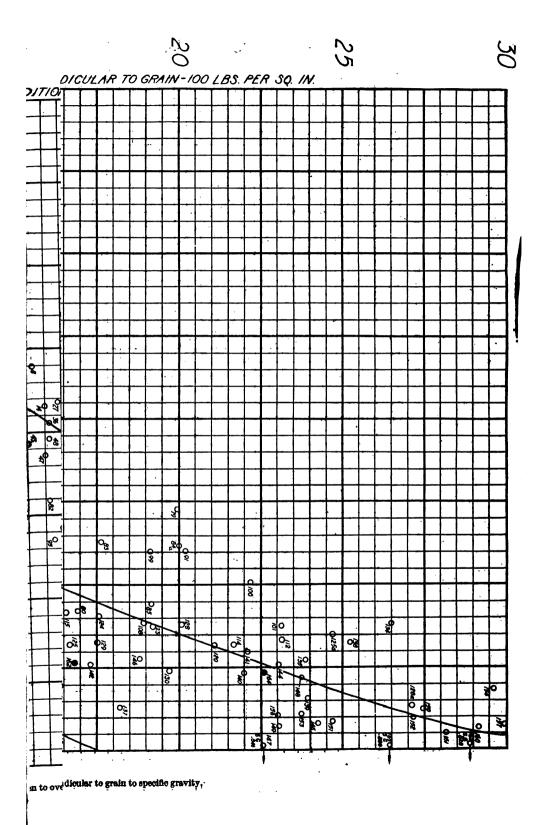
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### APPLICATION OF THE EQUATIONS.

Additional data may possibly necessitate the making of some slight changes in the equations given in Table 1 and the diagrams. However, for comparing species and for determining the best utilization of timber, the value of the equations as they are now is not affected by this possibility. It is to be expected that among a large number of species of widely different structure many will be found which do not satisfy very accurately the average equations connecting the various properties with specific gravity. It is often this variation from an average relation which determines the usefulness of a species for a special purpose.

As an example of the use to which the table and diagrams may be put, suppose it is desired to obtain the strength in compression parallel to the grain of a piece of green hemlock (eastern) grown in the southern Appalachian region. Its specific gravity may be determined by any one of several means which may readily be devised, and we will say that it is found to be 0.38. In the table, the "specieslocality" which is probably most nearly representative of the region in question is the eastern hemlock from Tennessee, and of this the maximum crushing strength is 29 per cent above the average for woods of the same specific gravity. To find what an average wood of a specific gravity of 0.38 will stand in compression parallel to the grain, we solve the equation  $C = 6,900 \times 0.38$ , or turn to figure 1 and read from the curve a maximum crushing strength of about 2,600 pounds per square inch. But since the compressive strength of the Tennessee hemlock was 29 per cent high, it is reasonable to expect that the timber in question will also run about 29 per cent high, or that the value would be about 3,300 or 3,400 pounds per square inch  $(2,600 \times 1.29 = 3,354)$ . Any of the other properties of the hemlock under consideration may be estimated in a similar manner.

Again, suppose it is desired to obtain a wood for a use which requires that it be very strong for its weight in its ability to resist a splitting force. Tension perpendicular to grain is the best measure of this. By looking down the column, "Tension, surface of failure radial," it is found that in ability to resist such a force, yellow buckeye is 17 per cent stronger when green and 120 per cent stronger when air-dry than is the average wood of the same specific gravity. It would appear at first that yellow buckeye is the most desirable wood for the purpose, but there is another consideration to be taken into account. Tension perpendicular to the grain varies with the square of the specific gravity; and it must be remembered that those properties (such as tension perpendicular to grain, hardness, work values, and compression perpendicular to the grain) which vary with the higher powers of specific gravity show a large increase in strength

with a comparatively small increase in specific gravity. For instance, a wood with twice the specific gravity of another would be expected to have four times as much strength in tension. Yellow buckeye is a very light wood and woods of more than double its specific gravity may easily be found. Such woods, even though they may run somewhat less in tension strength than the average wood of their weight, may have a tension strength considerably in excess of that of yellow buckeye. Thus, the red oaks, having a specific gravity of about twice that of yellow buckeye, are several times as strong in tension perpendicular to the grain, although they are very little above the average wood of their weight in this respect.

It may be seen from these examples that in comparing different timbers or species, in estimating their various properties, and in finding species with exceptional strength in some properties which may render them valuable for special uses, a knowledge of the specific-gravity strength relations is a valuable aid. It must be borne in mind, however, that such equations can never take the place of tests of species whose properties are unknown. If any particular mechanical property is known, the specific gravity may be approximated and the other properties estimated; even the properties of woods upon which no test data are available can be estimated with a fair degree of accuracy from the results of specific gravity determinations. Nevertheless, it is apparent from a study of the table and diagrams that no one kind of test can replace a complete series of tests.

### APPENDIX.

### METHOD OF DERIVING EQUATIONS.

In plotting the various points to a natural scale (i. e., the shrinkage or a given mechanical property vs. specific gravity) it was found that in many cases they arranged themselves in the form of a curve, or if their trend was along a straight line, this line would not pass through the origin. Assuming that the function should pass through the origin, i. e., that a piece of wood of zero weight or specific gravity should have zero strength, it was found that in practically every case a curve of the form  $f=pG^n$ (where f is the strength value, G the specific gravity, and p and n are constants) would fit the points quite well. This equation is the general equation of the parabola of the nth degree passing through the origin.

In order to simplify the determination of the proper values for the constants p and n the equation was transformed into the logarithmic form,  $\log f = \log p + n \log G$ . This equation represents a straight line having its slope equal to n and its intercept on the y axis equal to  $\log p$ . Consequently, to find the constants p and n it is only necessary to plot log f against log G on ordinary cross-section paper and find the straight line which best averages the points; then n and log p are determined from the slope and intercept of this line.

To find the straight line which best averages the points in the logarithmic plot the following plan was adopted:

By successive trials the parallel lines BB and CC (see fig. 9) were so located that 25 per cent of the points were above BB and 25 per cent were below CC and at the same time the vertical distance between the two was a minimum. Two lines (not shown on the figure) were then drawn as follows: Both parallel to BB and CC, one bisecting the distance between them and the other in such a position that 50 per cent of the points were on each side of it. AA was then drawn midway between these two lines and assumed to be the line which best averages the points and best represents the relation between specific gravity and the strength property in question. This method, as can readily be seen, is very likely to produce values of n such that the resulting equations can not be handled without the use of logarithms. As the slope of the lines could in most cases be varied through a considerable angle without appreciably affecting the distance between the lines BB and CC, the slope was so taken that a would be a fraction with the denominator 1, 2, 3, or 4. The solution of the equation is then possible by using the rules for the extraction of square and cube roots. ever it happened that more than one direction of the lines BB and CC fulfilled the conditions outlined above, preference was given to that slope which would simplify the form of the equation. The constant p was changed at the same time, so that the new line A1A1 passed as nearly through the center of gravity of the points as possible.

The analytical process known as the "method of least squares" can be applied to determining the mathematical relations between two properties of a substance as ascertained from experimental results. This method was used in one or two instances to determine the specific gravity strength relations; but it was found that the long and refined computations essential to the application of this method to so large a number of tests was not justified by the added accuracy of the final determinations. Especially is this true since it is desirable to obtain n to the nearest 0.125 only, and since undue refinement in the value of the constant p is unnecessary in view of the fact that there is a considerable variation of actual results from the values given by

any equation which may be derived.

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	Species and locality.		I.—EQUATIONS FOR SHRI	1	GreenGreen to oven-dry	Air-dry

II.-MEASURE OF ACCURACY OF RESPECTIVE EQUATIONS.

Proportion of species-locality.												Per	Percentage of equation value.	ge of	equat	ion v	alue.												
10 per cent above, per cent	1		:	119	128	121	123	114	121	139	149	149	118	122	135	142	130	119	133	136	121	121	0 119	9 117	7 130	134	135	140	
Der cent above,	<u> </u>	İ	•	91	116	109	112	108	113	117	8	 	110	109	121	118	115 1	111	117	115 1	110	111	109	9 108	9 118	116	118	127	_
per cent perow,	-	i	-	8	8	8	16	91	88	8	88	72	8	8.	28		<b>98</b>	8	88	 88				8	 8		8	74	
per cent perow,	-	İ		8	11	20	29	8	92	22	2	8	\$			- 92	23		-22	4	<u>'،</u> و	82	89	8	 		33	51	
10 per cent above,				i	i	:	128	113	123	164	139	167		130	143	145	145	116	142 1	133	131 124	120	0 125	122	144	151	139	141	
per cent above,		i	i	1	1	-	Ξ	901	110	135	117	130	112	110	125 1	120	127	108	130	118	115 111	1 112	2 112	110	128	121	127	122	
per cent below,	Ī	i	÷	1	:	:	8	88	8	75	æ	72	88	68	28	88	83			8	- <del>8</del>	<u>2</u>	90		-28	2.	<b>6</b>	88	
per cent below,		İ	i	i	Ī	•	22	8	8	8	8	88	æ	8	8	2			29	7	- 62		88	79 78	 		25		
III.—ACTUAL VALUE OF	LUE	OF 1	EACI	H PE	COPE	ACH PROPERTY		FOR EACH	ТСН	"SPECIES-LOCALITY" AS EQUATION VALUE.	EQU	LOC	ALIT ON V	Y",		DETERMINED	RMII	(ED	ву	rest	8—E	XPR	ESSE	TESTS—EXPRESSED IN	PEI	CEN	PERCENTAGE	E OF	-
Alder, red (Wash- ington): Green	8		1	119	125	117	21	119	83	139	131	102				117 1	136	117	138	8	137 111	119 128	S 108	8 110		138	139	137	
Ash, Biltmore (Tennessee): Green	8			. 8	87	8	77	116	201	142	104		120	011	130	86	123	114	103	135	121 121	125	124	110	611	100	106	86	
Ash, black (Michigan): gan): Green. Air-dry	8			122	118	103	12 52	130	9 100																				_
Ash, black (Wisconsin): Green Air-dry	2			- 13			\$8	107	25.25			162	88	88	88	•												801	
Ash, blue (Ken- tucky): Green. 99 Air-dry.	8			25	22	22	88	113	88	146	121	117	102	87 1 108 1	117 1	108	115	114	98	144 135	135   135 135   132	122	8 141 2 112	128	108	112	88	101	

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TABLE 1.—Equations and		Species and locality. Reference number.		III.—ACTUAL VALUE	1 2	Ash, green (Louisi- ana): Green Air-dry	son, pumpkin(Aus- souri): Green	Ash, white (Missouri): Green Air-dry
ns an	dry, based on of test.	Specific gravity, oven		E OF	623			
		Moisture content.	Per cent.	EACH	4			
ratro	Shrib gree dry	In volume,	Per		40'	98	87	88
138	Shrinkage from green to oven- dry condition.	Radial.	Per cent of di- fneusions when green.	PROPERTY	9		96	8
speci	from ven- tion.	Tangential.	of di-	CRTÝ	4		78	4
Jec gr		Fiber stress at elastic limit;	Lbs. per	r For	oo -	66	128	107
raviey	Sta	Modulus of rupture.	Lbs. per sq. in.		6	110	118	101
, sur	Static bending	Modulus of elasticity.	1,000s of lbs.	БАСН	10	102	110	88
nkag	nding	Work to elastic limit,	per cu. in.	EQU	Ħ	22.22	139	
e, an	• .	Work to maximum load.	per cu. in.	CIES	12	201	20,00	47.9
1a su	-	Total work.	Inch lbs.	V NC	13	77	25 25	
engr	Impa 30-pot	Fiber stress at elastic limit.	Lbs. per sq. in: 1,000s of lbs.	ALLI	14	112 191	 88 80	
n reu	act be	Modulus of elasticity,	per sq. in.	E-C	15	8.83	 288	
varianons—specylc gravny, snrinkage, and strength relations based on tests of small clear pieces, green and art-ary—Con	Impact bending, 80-pound hammer.	Work to elastic limit, Height of drop caus-	per cut, in.	SPECIES-LOCALITY", AS DET	16 1	137	102	
oas		ing complete isilure. Fiber stress at elastic	Lbs. per	ETEI ed.	17 18	888	25 E	
a on	Compression parallel to grain:	limit. Maximum crushing	sq. in.	DETERMINED nued.	19	108 113 91	126 115 105 97	
16818	sssion of to n:	atrength. Modulus of charicity.	sql lo s000,1		250	2 2 2 2 3 3 3	101	
9	niar to grain.	Compression perpendi	persq in Lbs, per sq in sq in	ву т	21	86.11	139	
matt		End surface.	Lbs.	ESTS	22	122	114	
скеат	Hardness: load required to embed a 0.44-inch ball one-half its diameter.	Radial surface,	L.bs.	TESTS—EXPRESSED	-83	105	118	119
риесе	s: red la ball tts	Tangential surface.	Lbs.	RES	53	107	124	112
s, gre	Вневг.	Surface of failure radial.	Lbs, per:		28	#H	128 23.58	134
sen a		Surface of failure tangential.	Lbs. per	IN I	38	102 83		112
na a	СІевувде.	Surface of failure radial,	Lbs.	PERCENTAGE	53	811 90	103	
r-ar		Surface 00 saliung fargential.	Lbs.	ENT	88	86	88	
Ĭ	Tension	Surface of failure Laber of failure	Lbs. per	AGE	68	## ##	100	125
₫ 1	ij	Jaimegnat	Lbs. per sq.in.	OF	: <b>.</b>	100 E	50 00	108

82	113	358	23	420	21 25 26	132	135 140	223	8	<b>2</b> 22	<b>2</b> .88	នដ
1122	117	142	2	135 101	103	117	102	901	8	8	5.5	142
88	117	558	8	135 131	140	130	88	119	88	85	<u>% ដ</u>	121
161	1118	500	22	<b>3</b> 8	92 191	115	97 821	28	87	88	88	88
100	88	119	88	<b>8</b> 171	00 100 100	103 158	108 98	100 101	28	8821	91 118	388
6110	135	23.53	87	114	104	101 150	88	103	82	13.2	85	82
117	27.75	118	83	22 88	828	93 115	95. 20.	83	26	107	8 101	828
138	222	112	85	<b>13</b> 00	88	88	104 98	86	1	<b>28</b> 25	8 2	요절
11 8	25	106 121	69	132	<b>3</b> 8	108 108	104	228	92	88 011	88	83
119	114	96 108	72	88	88	98 117	77	88	61	28	28	38
8.2	201 201	55 <b>2</b>	75	<b>7</b> 17 17 17 17 17 17 17 17 17 17 17 17 17	158 128	55	<b>6</b> 6	83	ĸ	101	88	23.53
1188	88	115 103	87	H21	102	28	28	<b>₹</b> %	8	88	នន្ទ	89
88	105 88	111	98	115 143	165	<b>ಟ</b> ಸ	107 67	28	8	276 109	28	82
81.8	ĦĦ	88	144	146	137	114 55	88	22	187	<b>2</b> 80	162	130
85	146 145	115 121	121	135 166	<b>8</b> 8	122	108 87	<b>7</b> 7	4	28	115	88
88	102	102	88	52	138	97 108	82	101	8	97 117	911	100
55	119 115	114 116	8	112	<b>3</b> 3.	62	25 28	88	82	81 132	99	28
HH	115	28	125	28.83	172 173	252	<b>8</b> 23	82	<del>1</del> 2	83	<u>स</u>	88
151	130	15	117	<b>5</b> 2	25	135 24	901 110 100	388	151	107	<b>44</b>	112
929	118	130	135	28	21.88	818	826	<b>88</b>	8	2821	82	2823
100	103	111	8	<b>8</b> 25.	127 127	106 157	88	22.83	<b>2</b> 2	102	107	117
===	108	113	8	111	11 108 115	ទីឧ	88	<b>58</b>	æ	105	85	97
255	107	116 118	8	1179	135 135	<u> </u>	88	88	2	88 119	88 88	8 72
8	2	88	113	132	178	156	# :	811	<u>8</u>	92	<b>x</b>	6
88	8	8	8	8	<b>2</b>	<b>8</b>	84	<u> </u>	147	£1 :	<u> </u>	152
- 8	8	88	8	7	<u> </u>	162	202	55	116	8	9 1	<u> </u>
									_ ; ;			
			:		•		011				<u>' ! ! </u>	
8	88	8	ន	ล	22	20		88	8	83	107	<b>8</b>
Ash, white (Arkan- 888): Green. Alr-dry.	Virginia): Green Air-dry Ash, white (New	York): Green Air-dry.	Aspen (Wisconsin): Green. Air-dry	Aspen, largetooth (Wisconsin): Green. Air-dry. Basswood. (Penn-	Sylvania): Green Air-dry Basswood (Wiscon-	Green Air-dry	Green	vania): Green Air-dry Birch, paper (Wis-	Green.	Birch, sweet (Pennsylvania: Green Alr-dry Birch, yellow	(Fennsylvania): Green Air-dry Birch, yellow (Wis-	consin): Green Air-dry

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	Species and locality		III.—ACTUAL VALUE OF	1	Buckeye, y e 11 o w (Tennessee): Green Air-dry	Green.	Butternut (Tennes- 800): Green. 27 Alr-dry.
	Reference number.		ALUI	2	0	. 848	153
-dry, based on of test.	Specific gravity, oven-		3 OF	60			
	Moisture content.	Per cent.		44.			
Shri gree dry	In volume.	Per	H P	10	127	22	109
Shrinkage from green to oven- dry condition.	Radial.	Per cent of di- mensions when green.	ROPI	9	113	88	87
from ven- tion.	Tangential.	of di- when	BRTY		141	18	105
	Fiber stress at elastic limit.	Lbs. per sq. in.	EACH PROPERTY FOR EACH	00	98	11	103
Sts	Modulus of rupture.	Lbs. per	EA.	6	100	85	818
vtic be	Modulus of elasticity.	1,000s of lbs. per sq. in.		10	115	25	20
Static bending.	Work to elastic limit.	Inch lbs. per cu. in.	SPE EQU	11	100	117	132
	Work to maximum load.	Inch lbs. per cu. in.	CIEB	12	109	 182	145
	Total work. Fiber stress at elastic	Inch lbs. per cu. in.	LOC.	13	1082	185	162 266 1
Impi 50-pot	limit.	Lbs. per sq.in. 1,000s of lbs.	ALIT	14	105	85	1001
act be	Modulus of elasticity.	per sq. in.	Υ Ε	15	112 107	92	118 122 1
Impact bending, 50-pound hammer	Work to elastic limit. Height of drop caus-	per cu. in.	"SPECIES-LOCALITY" AS DETERMINED EQUATION VALUE—Continued.	16	121 175	91	144
	ing complete failure.	Inches.	ETEI led.	17   1	90	157	148 151
Compression parallel to grain.	limit. Maximum erushing	sq.in.	SMIN.	18 1	88		128
ession el to in.	strength.  Modulus of elasticity.	sq. in.	ED 1	19 20	91 16	- <u>'</u> -	92 133 133 133
_	Compression perpendic	per sq. in.	ву т	- R	106 8138 18	70 114	55 94
	End surface.	sq. in.	EST	1 22	88 121 182 99		106
Hardness: load required to embed a 0.444-inch bal one-half its diameter.	Radial surface.	Lbs.	EX	23	1 9 94	90 112	6 108 105
Hardness: load required to embed a 0.44-inch ball diameter.	Tangential surface.	Lbs.	PRE	24	108	105	861
	entlace of sailure sailure failure	Lbs. per	TESTS-EXPRESSED	-8	122	118	881
Shear.	Surface of failure tangential.	L bs. per sq. in.	Z	-8	112	 &	22
Clea	Surface of failure fadial.	L.bs.	PERCENTAGE	23	618	88	889
Cleavage.	Surface of failure tangential.	Lbs.	CENT	88	139	8	157
Tension.	Surface of failure fadial.	L ba. per sq. in.	AGE	23	117	101	167
sion.	Surface of failure tangential.	Lbs. per sq. in.	OF	8	142	8	169

951	8 5	130	5 5 8	25.22	112	132	182	<u>; ;</u>	102	108	120
159	137		104	149	829	111	501 123	137	<u>\$</u>	8	121
92		128	132	8	==	94	28	ō	88	88	87 114
154	108	119		128	130	125	110	E	80	88	108
116	<u> </u>	117		58	82	201	EE		106	591	58
114		115		98	103	8	58	102	88	911	88
- 5		112		88	98	98	8.8	115	901	58	28
25	137	121	108	108	58	103	88	118 128	011	28	88
112	135	713	139	108	911	101	88	25	112	22	88
8	156 126	88	88	1105	107	8	88	328	90	8	88
<b>1 2 3 3 3 3 3 3 3 3 3 3</b>	2 8	35	88	82	80	138	25 <del>2</del>	67	8	=	28
901	106	8=	884	1282	82	8	<b>8</b> 10	88	16	8	<b>22</b>
115	**	===	96	1100	108	111	114	26	8	8	22
123	3 8	107	118	102 88	202	139	<b>Ξ3</b>	88	911	8	<u> </u>
22.5	3 8	818	195	108	132	144	99	28.88	7	128	128
911	2 8	505	107	99	84	134	127	<b>3</b> 15	87	88	5.2
104	011	110	882	88	2,8	119	601 87	222	83	28	52.2
171	108	35.	137 270	114	103	149	<u>58</u>	22	8	<u>\$</u>	## ##
149	123	55 5	110	104	28	118	119	228	111	6	137
130	169	102	174	110	100	121	24	84	4	8	22.4
91	36	. II	115	88	35	135	58	4.4	75	20	88
113	911	= = = =	88	83	843	Ħ	011 08 108	282	88	\$	25
108	119	103	88	97	82	111	133	8482	8	26	388
98	105	28	168	26	103	191	118	2	26	115	
107	911	83	81	8	8	061	22	116	116	8	
88	112	84	81	8	118	80	601	Ξ:	108	91	
				•							
7	8	22	8	\$	3	9	23	161		8	82
Butternut (Wisconsin):	Chinquapin, west- ern (Oregon): Air-Air-Air-Air-Air-Air-Air-Air-Air-Air-	Cherry black Chenry vania): Green		Obstruct (Tenner		(Washington): Green. Air-dre	Cucumber tree (Tennessee): Green Air-dry			(Ore-	Wiscon- athon

TABLE 1.—Equations and variations—specific gravity, shrinkage, and strength relations based on tests of small clear pieces, green and air-dry—Con.

	Species and locality.	
dry, based on	Reference number.  Specific gravity, oven- volume at time	
	Meisture content.	Per cent.
Shringreen	In volume.	Per mens
Shrinkage fron green to oven- dry condition	Radial.	Per cent of di- nensions when green.
rom ren- ion.	Langential.	
	Piber stress at elastic limit.	Lbs. per sq. in. Lbs., per
Stat	Modulus of rupture.	Lbs. per sq.in. 1,000s of lbs.
to ben	Modulus of elasticity.  Work to elastic limit.	per sq. in.
ding.	Work to maximum	per cu. in. Inch lbs.
	Total work.	per cu. in.
207	Fiber stress at elastic	per cu. in. L bs. per sq. in.
Impac -poun	limit. Modulus of elasticity.	1,000s of 1 bs.
t bend d ham	Work to elastic limit.	per sq. in. Inch lbs. per cu. in.
ling, mer.	Height of drop caus- ing complete failure.	Inches.
Con	Fiber stress at elastic limit.	Lbs, per sq. in.
npress trallel grain.	Maximum crushing strength.	Lbs. per sq. in.
g ç	Modulus of elasticity.	1,000s of lbs. per sq. in.
cular to grain, tic limit.	Compression perpendic fiber stress at elast	Lbs. per sq.in.
Har load r to er J.444-ij one-l	End surface.	L.bs.
Hardness: ad require to embed a 144-Inch ba no-half its diameter.	Radial surface. Tangential surface.	Lbs.
	emilal to esalud	Lbs. ner
Shear.	surface of failure	sq. in.
Cle	tangential.  Surface of failure surface.	sq. in.
Cleavage. Tension	Surface of failure tangential.	Lbs.
	Surface of iailure radial.	Lbs. per
<u> </u>	Surface of failure tangential.	Lbs. per

EACH "SPECIES-LOCALITY" AS DE' EQUATION VALUE—Continued.	SRTY FOR EACH "SPECIE EQUATIC	ICH PROPERTY FOR EACH "SPECIE: EQUATIC	CTUAL VALUE OF EACH PROPERTY FOR EACH "SPECIES-LOCALITY" AS DETERMINED BY TESTS-EXPRESSED IN PERCENTAGE OF EQUATION VALUE-Continued.
	SRTY FOR	CH PROPERTY FOR 3	TE OF

30	88	82 83 83	119 45
83	26	142 127	81
88	*	115	<u> </u>
22	201	128	151
8	26	88	92
25	26	110	82
22	108	28.	= 2
প্র	108	112	85 88
Ħ	61	112	901
12	95	48	88
8		2.83	88
<u></u>	97	106 97	\$2
82	**		<u>2</u>
12		102 105	156
91	- %	115 97	2,53
15	83		88
41	8	92 92	<b>2</b> 2 2
13	122		207
21	139	130 95 76 111	\$ 25
=	91	130 76	88
9	8	88 82	55
6	102	113 105	58
∞	8	118 84	188
2	22	107	100 108 108
9	88	8	8
10	88	. 89	8
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m			
-81	81	102	7.
1	Elm, cork (Wisconsin, Rusk County): (17): (170): (1	Eim, slippery (Indiana): Green Green Andrary Elm, slippery (Wis-	consin): Green Air-dry.

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138 98	126	22	121 76	88	252		142	121 2				
135	137		117	8	88		<b>₹</b> 5	3 8				-
132	112	51	115	8	130		142	. 75				
132	13.8	19	119	12	108		157	3 22 8				
120	87 110	100	116	116	105		108	55	98	85 112	8815	8
. 122	<b>2</b> 80	82	105 89	86	103 98		===	85	. 8.8	88 107	27.	91
110	1020	8 3	95 20 20 20 20 20 20 20 20 20 20 20 20 20	114	117		110	1 88	100			
86 86 80 80 80 80	88 106	22	96 10 10 10 10 10	123	89 89		114	8 8	108			
100	82	86	112 114	102	113		<b>1</b> 012	828	104			
85	18	88	119 122	81	28.65		85	<b>8</b> 8 5	98	90 108 108	117	88
102	126	127	228	128	22.83		₹8	262	28	26	88	æ
88	. 22	180	88	121	88	8	3.8	. 2%	282	88	83	96
95	88	118	2.8	129	88	113	88	8 28	8	92	48	. 8
821	112	48	22	12	7.19		146	137	8	156	210 138	135
999	135	8 2	117	8	22		23 5	18	94	114	114	122
82	978	139	98	128	28		88	¥ 2,8	92	107	<b>7</b> .88	28
96	108	131	1505	107	82		92		:	111	101	88
128	142	88	77		8%		85	88	418	128	191	142
182	149	55	883		8.8		174			156	88	82
121	2.2	174	117	114	22 %		28.8	- F	38	114	8.8	88.4
88	97	142		126	22,22	105	64	5 <b>2</b> 8	35	103	88	88
104	107	132	78	107	క్రౌజ	<b>8</b>	8.5	 3 28 88	8.38	113	88	
- 88	83	179		128	\$2		4.2	18 5	28	117	84	88
- 81		8	86	143	86		\$	8				
		76	91	127	6		88	901				
112		57	105	—— <u>.</u>	8		털	8				
128	23	165	8	147	8		<u> </u>	% 24	971	138	151	138
'Ivania): Green Air-dry	n, white (wis- nish): Green Air-dry	enneart: Green Air-dry.	Gum, black (Ten- ness ee): Green	Gum, b lue (California): Green Air-dry	n, cott on (Lou- lana): Green Air-dry.	Green. Green.	fackberry (Indi- ana): Air-dry	kberry (Wis- nsin): Green Air-dry	Haw, pear (Wisconsin): Green Air-dry Hickory, big shell-	bark (Mississip- pi): Green Air-dry. Hickory, big shell-	dreen Air-dry	hio): Green 139
y white (Penn- drania): Green Air-dry	n, wand (wishing): Green Air-dry.	10 C	lack (	2) eg	tton (	d (K	kberry (Indi- la): Green	e e l	eer ( Lry big	Muss n lry big s	Obio) n lry	ry.
Elm, white (Pennsylvania): Green Air-dry	consin); Green Air-dry	Greenneart Green Air-dry.	m, black ess ee): Green Air-dry.	Gum, b lue (California): Green	um, cot islana): Green Air-dr	E. 3. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7.	Hackberry ana): Green.	Hackberry consin): Green	Haw, pear (Wisconsin): Green Air-dry Hickory, big shell-	bark (M) pi): Green Air-dry. ickory, bi	ark (Ohi Green. Air-dry	(Ohio): Green
<b>5</b>	10	5	Gr.	Gü.	Gu	5 2 2	e d	a o	H SH	r iii	م با	40

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igo	Surface of failure tangential.	Lbs. per	O.F	8		: :	
Tension.	Surface of failure radial,	Lbs. per		8			8
386.	Surface of failure fangential.	Lbe.	PERCENTAGE	88			
Clesvage.	Surface of failure radial.	L.bs.	ERC	27			
Shear.	Surface of failure tangential.	Lbs. per sq.in.	N N	26	107	25	
Sp.	erulisi lo sostrud Lisiber	Lbs. per sq.in.		25	8.88	84	
ss: ired la ball its	Tangential surface.	Lbs.	TEST8—EXPRESSED	75			
Hardness: load required to embed a 0.444-inch ball one-half its diameter.	Radial surface.	rps.	EXP	23			
Doed 10 444 on one of the	End surface.	Lba.	18. 18.	22			
niar to grain, ic limit.	Compression perpendid	Lbs. per sq. in.	TES	22	1117	88	
	Modulus of elasticity.	1,000s of lbs.	BY	20	96	72	8
Compression parallel to grain.	Maximum crushing strength.	Lbs. per sq. in.	AS DETERMINED BY ontinued.	19	109	28	. 911
Com	Fiber stress at elastic limit.	Lbs. per sq.in.	RMI	18	86	86	130
18. 10.	Height of drop caus- ing complete failure.	Inches.	JETE ued.	17	86	196	
Impact bending, 50-pound hammer	Work to elastic limit.	per cu. in.	AB I ontin	91	142 81	කික	
pact b	Modulus of elasticity.	1,000s of lbs.	E."	15	104	88	
In 50-06	Fiber stress at elastic limit.	Lbs. per	ALE	14	126	88	
•	Total work.	Inch lbs.	ON O	13	113	135	
வ்	Work to maximum load.	Inch lbs.	"SPECIES-LOCALITY" AS DET	123	118	168	127
andin	Work to elastic limit.	Inch lbs.	EQE EQU	=	104	22	8
Static bending	Modulus of elasticity.	1,000s of lbs.	1	10	107	101	113
ž.	Modulus of rupture.	Lbs. per	PROPERTY FOR EACH	0	110	101	114
	Fiber stress at elastic limit.	Lbs. per	F01	oc.	107	100	=
from ven- tion.	Tangential.	of di-	RTY	1-			
Shrinkage from green to oven- dry condition.	Radial.	Per cent of di- mensions when green.	OPE	9			
Shrin greed dry	In volume.	Per mens		10-			
	Moisture content.	Per cent.	EACH	4			
ry, based on of test.	Specific gravity, oven-d emij ta emulov		OF ]	80			
	Reference number.		LUE	8	144	159	166
	Species and locality.		L-ACTUAL VALUE OF	1	Hickory, mocker- nut (Mississippi): Green. Air-dry. Air-dry. mocker- mit (Pennsylva.	nia): Green Air-dry	Hickory, mocker- nut (West Vir- ginia): Green

		•				. ,				oo -≠+	7	
										128	47	
										95	88	
					_ <u></u>	_!!				132	23	
										102 113	2	
8	102	113	78 78	88	91	88	26	88	101	114	22	113
801	8	88 125	88	88	122	26		28.22	102	88	2	116
				<u> </u>						119	85	118
	!!_									114	8	117
										112 121	92	112
21 20 20 20 20	114	108 102	86	22	22.22	88	2	88	117	100 100	11	108 85
88	83	8	9 <u>1</u>	<u>\$</u>	<u>8</u>	<b>8</b>	22	105	##	88	22	62
27.88	113 98	105	105	<b>2</b> 288	121	88	95 95	108 108	112	23	82	101
# :	82	102	105	84	115	2	76	95	8	38	8	23
130	150	182	196	110	97	174 119		88	101 108	144 76	128	57 79
138	125	138 87	90	146	115 85	<b>8</b>		110 87	102	116 104	28	81
*	88 112	222	97 10 <u>4</u>	95 115	100	25.62	_ ! !	98	93 107	72	\$	22
115	114	105	112	131	111 88	85		114	104	88	28	8.5 25
149	121	522	138	132	130 128	149	146	121	98	114 40	92	88
169	145 114	10 <u>1</u>	182	128	97	190	22	114	111	100	8	5.8
28	102 79	108	88	48	201 201 201	88.	121	22	88	95	74	<b>451</b>
88	106	110	88	102	107	88	88	108	111	71	74	88
101	##	100	22	20.22	114	103	115	100	1103	22	88	88
8.6	112	110 87	8.6	22.22	112 94	91	\$ 8	101	103	78 81	2	21.88
										#:	88	22,
										\$	135	96
										11	107	18
112	148	157	<u>8</u>	161	0 <del>1</del>	152	143	153	₹ :	84	149	145
			ii ;;	a):	ark	ark	ark	a):	98	5		텵
ippd):	, ptg.	y.	lvani y y pig	irgin y shagb	(ippi): y shagb	Sahag	lvani y shagb	rgin y.	ppt): (meri	3ee): V		noun 300): 7
(Mississippi): (Green Air-dry Hickory	(Mississippl): Green Air-dry Elckory, pignut	(Ohio): Green Air-dry. Hickory, pignut	ennsy Freen Vir-dr kory	(West Virginia): Green Air-dry. Hickory, shagbark	(Mississippi): Green Air-dry. Hickory, shagbark	(Ohio): Green Air-dry. Hickory, shagbark	Pennsylvania): Green Air-dry kory, shagbark	(West Virginis): Green. Air-dry. Hickory, water	(Mississippi): Green Air-dry Holly, American	(Tennessee): Green. Air-dry. Hornbeam (Ten.	nessee): Green Air-dry	Laurel, mountain (Tennessee): Green Air-dry
HIS H	H	E S	(Pennsylvania): Green Air-dry Hickory, pignut	E E	Hick C		Hick C.	H is	(Mississippi): Green Air-dry Holly, American		nes	I E

TABLE 1.—Equations and variations—specific gravity, shrinkage, and strength relations based on tests of small clear pieces, green and air-dry—Con.

			. Fe		. 83 8		
Tension.	Surface of failure tangential.	Lbs. per	E OF	8	82 21	<u>:                                      </u>	102
	Surface of failure failers.	Lbs. per	[AG]	88	88 63 114	= = = = = = = = = = = = = = = = = = = =	₫.
88	Surface of failure tangential.	Lbs.	EN	88	28 28 22 24	2	켴
Сіевта <b>д</b> е.	Surface of failure radial,	Lbs.	PERCENTAGE	22	71 58 96	112	89
j,	Surface of failure tangential.	Tog. pol sq. in.	ZI.	88	100 123 119	103	9
Shear,	Surface of failure radial.	Lbs. per sq.in.	SED	28	133 107 115	108	8
s: red ball ts	Tangential surface.	Lbs.	RES	22	114 93 125	2,	8
Hardness: load required to embed a 0.444-inch ball one-half its diameter.	Radial surface.	Lbs.	TESTS-EXPRESSED IN	83	102 86 128	22	163
Egg 545	End surface.	Lbs.	TR	য়	100 61 114	105	90
ic limit.	Compression perpendicularies at elast	Lbs. per sq. in.	TE	12	130 119 132	28	8
1.00	Modulus of elasticity.	1,000s of lbs. per sq. in.	"SPECIES-LOCALITY" AS DETERMINED BY EQUATION VALUE—Continued.	8	102 168 78	8	78
Compression parallel to grain.	Maximum erushing strength.	Lbs. per sq. in.	INEI	19	149 117 104	84	88
Com	Fiber stress at elastic limit.	Lbs. per sq. in.	ERM	18	155 111 100	85	8
ig, ier.	Height of drop caus- ing complete failure.	Inches.	DET.	11	110 110 76	88	86
hamn	Work to elastic limit.	Inch lbs. per cu. in.	AB	91	121 84 61	28	6
Impact bending, 50-pound hammer	Modulus of elasticity.	1,000s of lbs. per sq. in.	TE-C	91	120 105 99	88	8
100 100	Fiber stress at elastic limit.	Lbs. per sq. in.	CAL	14	130 97 87	74	84
	Total work.	Inch lbs. per cu. in.	B-LO ON	13	80 125 83	94	<b>5</b>
50	Work to maximum load.	Inch lbs. per cu. in.	ECTE	71	88 102 79	2	æ
Static bending.	Work to elastic limit.	Inch lbs. per cu. in.	rgP EQU	11	164 124 71	=======================================	121
attic b	Modulus of elasticity.	1,000s of lbs. per sq. in.	EACH	01	115 101 96	22	57
ž.	Modulus of rupture.	L bs. per sq. in.		6	130 113 101	87	86
	Fiber stress at elastic limit,	Lbs. per sq. in.	ACH PROPERTY FOR	œ	148 115 88	86	88
from ren- lon.	Tangential.	f di-	ERTY	2	62	128	81
Shrinkage from green to oven- dry condition.	Radial.	Per cent of di- mensions when green.	ROP	9	20	101	8
Shrin greet dry c	In volume.	Per o	н ы	9	55	108	108
	Moisture content.	Per cent.	EAC	4			
ry, based on f test.	Specific gravity, oven-d-	,	OF	9			
	Reference number.		LUE	8	158	101	128a
	Species and locality.		IIIACTUAL VALUE OF	1	Locust, black (Tennessee): Green Air-dry Locust, honey (Indians): Green	Madrona (Califor- nia): Green	)regon):

121   156   135   138	132 151	122 132 66 104	135	149	108	74	::	<del>දි</del> ස	119	108	102	28
121		82				-	- 1 1		_ :	-	. AA	30
		: =	102	83	106	25		98	95	88	8	28.28
157 119	4	139	261	132	132	711	104 138	72	113	100	102 95	102
113	126	119	8 85	132	112	108	36	2 <b>.</b>	108	25	25.	8.4
115	123	120 135	115	124	119	115	115	52,8	5	109	28	88
33	122	109	85 <u>4</u>	116	105	107	109	88	8.	100	88	168
522	121	110	85 102	112	110	108 116	28 107	110 94	901	105	18	200
128	121	102	85 101	112	108	108	8 5 <u>1</u>	80 <u>1</u>	108	108	8.8	98
119	130	114	90.	112 145	821	108	89 112	25 25	106	88	648	22
113	121	88	528	95 100 100	88	88	104 92	102 79	116	110	23	77
127	8	119	88	28.38	2.8	22,88	86	59	89	78	22.82	88
28.28	107	97	101 101	82.83	100	101	103 101	28.2	75	26	22.22	88
88	86	97 114	88	81 128	84.88	98 117	8	88.88	\$	8	88	8%
88	22	28	83	550	84	88	32	28.28	&	7	833	88
103	88	118	146 113	92 171	102 76	91	<b>3</b> 2	28 20 20	88	32	88	<del>1</del> 8
25.8	110	102	95	. 88	85.8	82	\$\$	88	æ	*8	101 119	86
861	8	110	11.9	83	52.22	116	<u>ਬ</u> ੜ	27.	<b>2</b> 5	75	<b>%</b> 101	28
25.25	73	88	88	52	25.52	22	888	67	3	46	នន	5 6
187	108	812	88	25.88	88	58	88	22	r.	4	64 68	88
88	146	78 130	~~~~~~ % <b>2</b> 2	88	88	田器	22	22	8	\$	64	84
28	86	118	55.20	28.23	88	<u>§</u> 8	88	22.22	8	2	88	28
88	110	82	28	83	58	53.3	85	82	75	88	88.	<b>38</b> 55
28	1117	94 113	55 88	82	95	107	28	88	75	95	88	8.8
28	95	108		6	88	6		8	4	119	8	16
প্র		8		.22	25	5		8	<b>88</b>	119	101	ğ
88	8	95		8	8	8		4	81	8	108	114
	:											
						108						
8		8	83	28	52		124	128	8		121	133
Magnolia (Louisi- ans): Green Air-dry.	Waple, Oregon (Washington): Green	Maple, red (Pennsylvania): Green Air-dry.	Maple, red (Wis- consin): Green Air-dry	maple, sirver (wisconsin); Green Air-dry Maple, sugar (Indi-	ana): Green Air-dry Maple, sugar (Penn-	Sylvania): Green Air-dry Maple, sugar (Wis-	Green. Air-dry	sin): Green Air-dry	Osk, Calliornia black (California): Green. Air-dry	Oak, canyon live (California): Green	Oak, chestnut (Ten- nessee): Green. Air-dry Oak, cow (Louis-	iana): Green Air-dry

		no bes		Shrin	Shrinkage from	from		ů	d d	Stotio bonding			Impa	ct per	Impact bending,		Compression	ssion	aist3,	E Se H	Hardness: oad required to embed a	ired	S. Pool		Cleawage		Tenefon
		dry, ba of test.		dry	dry condition.	tion.		5				<del></del>	50-por	म् वृ	mmer	<del>.</del>	grain.	3 -	tic limi	0. 8 8 9	0.444-inch bal one-half its diameter.	ball its ir.				:	
Species and locality.	Reference number.	Specific gravity, oven- volume at time	Moisture centent.	In volume.	.laibaA	Tangential.	Fiber stress at elastic limit.	Modulus of rupture.	Modulus of elasticity.	Work to elastic limit.	Work to maximum load.	Total work.	limit.	Modulus of elasticity.	Work to elastic limit. Height of drop caus-	ing complete failure.	limit. Maximum crushing strength.	Modulus of elasticity.	Compression perpendic	End surface.	Radial surface.	Tangential surface.	Surface to salung salung fails.	Surface to soluted familiars. Surface to soluted to soluted to soluted to solute to so	emist to sostma faibar emist to sostma	fangentlal.	Burtace of failure tangential.
			Per cent.	Per mens	Per cent of di- mensions when green.	<del></del>	Lbs, per sq.in.	Lbs. per	1,000s of lbs. per sq. in.	Inch lbs. per cu. in.	Inch lbs. per cu. in.	per cu. in.	19 ps 19 ps 1 sq. in. ps 1 sq. in. ps 1 sq. in.	per aq. in.	per cu. in.	Lbs. per	sq.in.	1,000s of lbs.	Lbs. per	Lbs.	Lbs.	Lbs.	Lbs. per sq. in.	Lbs. per sq.in.	rpe.	Lbs. per	sq.in.
III.—ACTUAL VALUE OF	LUE		EACH		PROPERTY	RTY	FOR	EACH	<b>, H</b> O		UAT	LOC	SPECIES-LOCALITY" EQUATION VALUE-		AS DETE Continued	TER ued.	DETERMINED	3D BY		STS-	EXE	TESTS—EXPRESSED		IN P	PERCENTAGE	NTA	GE OF
1	64	62	70	70	9	1	œ	6	10	11	12	13	14	15	16 17	- 18	- 61	8	2	23	23	234	25	56	22	88	20 30
Oak, laurel (Louis- iana): Green.	116			119	E	66	188	88	8.8	2.2	88	25	88	8015	828	85	888	2,2	885	102	112	011	88	781	182	35	194
Oak, post (Arkan- 8as): Green	130			93	101	105	88	27	58	110	88	88.4		8 5						22	5 5 8	<u> </u>	3 28	28			
Oak, post (Louis- iana): Green Air-dry	137			95	16	58	88	830	22	<b>6</b> 4		28								100	911	218	88	8 8			
Oak, red (Arkansas): Green	119			91	78	88	12	88	86	8	100	101	93	92	- 6	94 78	- 88	82	107	110	114	114	101	-2		107	108

•	REI	LATIO	N OF	SHRI	NKAG	е, ет	C., T	SPI	ECIFIC	GRAVI'	ry.	25
98	107	121	82	<b>25</b>	101		135 101	00 108	93	119 87	108	1138
202	9	114 85	83	72	88		528	84	28	88 %	\$\$	117
112	92,4	222	88	252	38		101	88	93	102	22.88	112
105	102	116	528	82	88		\$ <u>5</u>	<u>\$</u> 8	48	22 12	<b>82</b>	116
28	28.82	88	83	\$8	28		58	83	100	86.66	88	88
27.22	48	22.52	97 59	88	38		55 58	91 88	91 103	88	2,8	100
108	10 <u>4</u>	107	95	\$E	28		114 85	87 106	2 8	105 84	101	90.
518	\$7.8	112 98	104	ឌ្ឌឌ	98		116 95	88	55.8	108 83	104 18	<b>2</b> 2 <b>8</b>
108 81	96	95 8	100 71	108	88		81 81	88	22	97	88	88
88	88	22	98	132	28.62	169	98	88.	84	108 141	<b>8</b> 9	110
88	119 92	22.82	92 179	117	23.83		111	84	88	\$8	88	88 22
48	83.88	<b>2</b> 8 8 8	22.23	H H	82	128 108	88	88	88	<b>3</b> 8	82	78
5.5	28	92	Ę2	101 101	84	147	828	<b>88 8</b>	388	88	88	76
812	882	121	88	58			<b>88</b> 88	83	87	88	26.02	
28.58	88 116	88	28	<b>8</b> 01	33		88	8.73	84	82	19 19	113
88	107	95	58	113	88		825	88	100	88	25.28	. 88
28	88 EE	101	88	95	884		55.88	<b>2</b> 2	\$ 28	2%	22,5%	<b>25</b> 5
128	28	88	84	23	88		22	28	8.3	188		78 %
48	24	88	67.8	<b>\$</b> 10	88		83	88	72	88	58	44
23.3	838	28	2.2	228	61		뒃쬬	23	84	<b>48</b>	58	82
<b>88</b>	258	88	<b>88</b>	113	55.88	<b>9</b> 9	1189	84	88	88	<b>%</b> 8	 88
 %%	88		28	100	<b>≇</b> ã	118	85	<b>2</b> 23	88	85	88	<u> </u>
88	38	28	28	110	88	평용	238	88	88	<b>≅</b> £.	101	<b>88</b>
84		8	88	혈	86		8	88		8	22.	101
8		4.	8	8	88		8	8	8	22	8	<u>a</u>
88		ឌ្ន	3	8.	8		102	8	88	8.	8	
118	117	26	22	142	S .	115	<b>H</b>	132	138	136	<u> </u>	<u>8</u>
(arra):	9	8	na): Span-	nā): Thite	Çeli-	è illo	rkap	Ę	Rich-	Mil.	a a	
Oak, red (Indiana): Grean	inna): Green Air-dry. Oak, red (Tennes-	966): Green Air-dry	ish (Louisiana): Green Air-dry Oak, lowland Span-	ish (Louisiana): Green Air-dry. Oak, swamp white	(Indiana): Green. Air-dry. Oak, tanbark (Cali-	Oak, water (Louis-	Jana): Oreen Air-dry Osk, white (Arkan-	Sas): Green Air-dry. Oak, white (Indi-	ana): Green Air-dry. Oak, white (Rich- land Parish	Louisiana): Green Air-dry Oak, white (Winn	iana): Green Air-dry. Oak, willow (Louis-	ne): Green Air-dry
A A Line	Great Great Air ik, re	Gree Gree Altr	[편 다 <b>8</b> 전 한	B. G. A. F. B. F. W.	Greek, ter	Green Air-dr	Gree Oree Air-	883): Gree Air- Sk. ♥J	una): Green. Air-dry ik, white	Louisiana): Green Air-dry ak, white (	Gree Gree	Green):
ō ö	ိ	Č	o o	ె ర్	ଁ ପଁ		్ రో	~ రి	~ . <b>5</b> ~	ొం	~ ō	,

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		-dry, based on of test.		Shrir greed dry (	Shrinkage from green to oven- dry condition.	from ven- don.		St gt	Static bending	nding	_		Imp 50-por	act be	Impact bending, 50-pound hammer.		Compression parallel to grain.	ession el to in.	rular to grain,		Hardness: load required to embed a 0.444-inch ball one-half its diameter.	ss: ired da ball its er.	Shear.		Cleavage.	9ge.	Tension.	lon.
Species and locality.	Reference number.	Specific gravity, oven- emit ta emuloy	Moisture content.	.emnlov nI	Radial.	Tangential.	Fiber stress at elastic limit.	Modulus of rupture.	Modulus of elasticity.	Work to elastic limit.	load.	Total work. Fiber stress at elastic	limit. Modulus of elasticity.		Work to elastic limit. Height of drop caus-	ing complete failure. Fiber stress at elastic	limit. Maximum crushing	strength.  Modulus of elasticity.	Compression perpendic	End surface.	Radial surface.	Tangential surface.	eurlish to sostume faibst	Surface of failure tangential.	Surface of failure radial.	Surface of failure tangential.	Surface of failure radial.	Surface of failure tangential.
			Per cent.	Per c mens	Per cent of di- mensions when green.	<del></del>	Lbs. per sq. in.	Lbs. per sq. in.	1,000s of lbs.  per sq. in.  per sq. in.	per cu. in.	per cu. in.	per cu. in.	ni .ps	per sq. in.	per cu. in.	Teq .edJ	sq.in.	1,000 soft lbs.	per sq. in. Lbs. per sq. in.	Lbs.	L.bs.	Lbs.	Lbs. per sq.in.	Lbs. per sq.in.	Lbs.	Lbs.	Lbs. per sq.in.	Lbs. per
IIACTUAL VALUE OF	LUE	O.F.	EACI	H PR	OPE	RTY	EACH PROPERTY FOR BACH	EAC		SPE(EQU.	ATIO	LOC	ALTI ALU	- Co	"SPECIES-LOCALITY" AS DETERMINED BY TESTS-EXPRESSED EQUATION VALUE-Continued.	ETE!	NIMS	ED 1	3Y T.	ESTS	E X	PRES	SED	Z	PERCENTAGE OF	ENT	AGE	0
1	94	09	4	10	9	1	00	0	10	77	61	100	14	15	16 1	17 18	8 19	8			81	74	ĸ	8	27	88	8	န
kansas); Green. Green. Ar-dry.	122			88	8	100	100	28	88	105	\$28	8.8	325	88	83 11	98 8 116 8	808	8 8 80	2112	528	110	528	98	91	107 81	411 94	119 85	128
Consin): Green	105					- 1	158	282	188	66	102	95 1	108	74 1	150	888	18.0		110		92	85	110	105	861	88	28	:
Osage orange (Indiana): diana): Afrens	164			42	42 107			105			_		8 8		- 4						131	901				3	1	

	F	RELAT	ON	OF SH	BINK	AGE,	ETC	., то	SPEC	CIFIC	GRA	VITY.	27
	81 192	119	125 110	2	<b>8</b> 8	136 55	<u> </u>	166 110	146	135 174	185 143	106	
	128 118	8.	149	26	93	131		137	107	125	161	8	
-	166	8	112	18	135	132		128	83	132	158	101	
	125	22	151	2	1138	128		116	112	83	22.42	110	
-	116	112	22	82	518	110		115	106	108 105	887	112	*
	102	011	121	22	112 91	106		258	3.6	\$ <b>2</b>	8 2	106	*
	22	130	114	88	88	8 2	919	114	쳝혈	12 12	121	128	H
	88	123	123 123	88	<b>8</b> 8	101	913	107 95	న్లో	114	114	128	108
	201 88	21	27 8 8	28	102	106	112	112	108	118	<b>2</b> 011	110	100
	102	135	113 164	88	858	<b>1</b> 01 10	101	882	28	88	183	8	101
	144 171	81	67.	8.19	104 118	130	75	88	55	115	<b>2</b> 24	119	95
	102	8 8	88	9.6	8,88	843	83	\$ 8	\$3	95	82.88	88	88.77
	102	8	20 20 20 20 20 20 20 20 20 20 20 20 20 2	80	<b>88</b> 101	<u>*</u> \$	129	13	88	25 25 25 25 25 25 25 25 25 25 25 25 25 2	22 52	8	101
	841	84	146 132		58	95 S		~~~ %å	82	927	272 118	144	28
	202	36	127	28.88	128	107		<u>5</u> 2	<u>5</u> 4	113	<b>1</b> 000	101	21
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	127	78	<b>88</b>	88	1188		83	86.2	58	117	57	102	88
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	9	132	8	107	86	131		911	611	115	8	4	
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									- 11				
				156									114
	8	88	126		49	8	19	8	ક્ર	3	#		11
Poplar, yellow (tulip tree) (Tennes-	Green. Air-dry. Rhod o d e n d r o n,	great (Tennessee): Grean Air-dry Eassafras (Tennes-	Green.	nessee): Green. Afr-dry. Silverbell-tree (Ten-	Green Air-dry	see): Green Air-dry Sumac. staghorn	(Wisconsin): Green Air-dry	Sycamore (Indiana): Green Air-dry	See): Green. Air-dry.	(Tennessee): Green. Air-dry	willow, diack (wis- consin): Green	Willow, western black (Oregon): Green	Witch hazel (Tennessee): Green Air-dry

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ss: I a Dall Its	Tangential surface.	Lbs.	RESS	22			611	:
Hardness: load required to embed a 0.444-inch ball one-half its diameter.	.eoaims laibasī	Lbs.	EXP	ĸ		•	919	20
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cular to grain,	Compression perpendic	Lbs. per sq. in.	TE	12			142	149
sion to	Modulus of elasticity.	1,000s of lbs. ni .ps 19q	D BY	8			117	135
Compression parallel to grain.	Maximum crushing strength.	Lbs. per	"SPECIES-LOCALITY" AS DETERMINED BY EQUATION VALUE—Continued.	19		121	130	135
Co	Fiber stress at elastic limit.	L bs. per	ERM	18		159	157	160
ing, mer.	Height of drop caus- ing complete failure.	Іпсрез.	DET nued.	11			119	Z Z
bend bam	Work to elastic limit.	Inch lbs. per cu. in.	, AS Conti	16		'	139	82
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	Fiber stress at elastic	Lbs. per	VAL	14		<u> </u>	116	133
	Totsi work.	Inch lbs.	SS-LC ION	13			88	011
<b>1 1 1 1 1 1 1 1 1 1</b>	Work to maximum load.	Inch lbs. per cu. in.	ECLI	12			88	121
bendi	Work to elastic limit.	Inch lbs. per cu. in.	"SP EQ	=			146	190
Static bending.	Modulus of elasticity.	1,000s of lbs.	ЕАСН	10		88	100	42
202	Modulus of rupture.	Lbs. per		6		115	55.8	124
	Fiber stress at elastic limit.	Lbs. per	PROPERTY FOR	<b>∞</b>		138	418	140
Shrinkage from green to oven- dry condition.	Tangential.	Per cent of di- mensions when green.	ERT			<u>:</u>	85	<u>1</u>
inkage en to cond	Radial.	Per cent of di- mensions when green.	ROP	9	-	-	88	8
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dry, based on	Specific gravity, oven- volume at time		OF	es .				
	Reference number.		LUE	8		8	~	ន
	Species and locality		III.—ACTUAL VALUE OF	1	CONIFERS.	Cedar, incense (California): Green.	Cedar, western red (Montana): Green	Cedar, western red (Washington): Green. Air-dry

Coder white (Wie	_	_	-		_	_	-	-	-	-	-	-	-	_	-	-	_	_	_	_	_	_	-	-	•	•	٠	
consin):	_			ă	ķ	ď	=	2													8	8	ž	-	4			Ş
Air-dry	<u>.</u>			8	?	2	18	32	8 6	38	130	2 4	38	100	128 128	107	102	88	18	34	88	84	8 11	38	33	3 5	25	18
Cypress, bald (Lou-	_																											
Green	29	-	-	91	88	28	117	105	228	135	200	<b>F</b>	7,5	901	86.	81 141	1 127	134	115	33	67	67	282	\$:	22	29	19	8
Douglas fir (California):			:		:		1	3		3		<u> </u>									g	8	ē	š	3	8	<del>-</del>	3
Green	458	:	-	102	118	102	128	114	133	128	<b>8</b> 8	2	113 1	130 11	110	92 27	7 123	182	114	ā	88	101	102	32	19	ĸ	29	62
Douglas fir(Oregon):	678			2	2	3	- 2	Ē	- 7	<u>:</u>	. 4	<u> </u>	- 40		: 8	- 2	136	<u> </u>	2	5	8	8	: 8	: 8	۶	8	. 8	: \$
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Douglas fir(Chehalis County, Wash-																											<del></del>	
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Douglas fir (Lewis			-				-	<del>-</del>	<u>:                                    </u>	-	<u> </u>	<u>:                                     </u>	<del>! _</del>	<u>:                                    </u>	<u>:                                    </u>	<u>:                                    </u>	-	:	:								<del>: -</del>	:
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Douglas fir (Wash- ington and Ore-								•																				
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Douglas fir (Wyom-				<u> </u>		-		-	-	-	<u>:                                    </u>	<del>: -</del>	<u>:                                     </u>	<u>:</u> :	<u>:                                    </u>	:	<u>:                                    </u>	<u>:</u>	<u>:</u>				-	<del>-</del>			<del>:</del>	i
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Green.	*			110	:23	137	182	102	82	110	<u> </u>	284	- 26	138	110 67	108	86	88	154	125	88	117	102	112	22.			į
Fir, amabilis (Ore-	_				:		3	=				3			_					<u> </u>	≩	*	3	3	1	3	<del>-</del>	:
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Fir, balsam (Wisconsin):	_										_																	
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		dry, based o	-	Shri	Shrinkage from green to oven- dry condition.	from ven-		Sta	Static bending.	guipu		ri)	Imps 0-bon	nd be	Impact bending, 50-pound hammer.		Compression parallel to grain.	ession el to in.	isig of rain		load required to embed a 0.444-inch bal one-balf its diameter.	fuired a bal litts ter.		Shear.	Cles	Cleavage.	Tension.	don.
Species and locality	Кебетенсе патрет.	Specific gravity, oven-	Moisture content.	In volume.	Radial.	Tangential.	Fiber stress at elastic limit,	Modulus of rupture.	Modulus of electicity.	Work to elastic limit.	,beol	Total work.	,timif	Modulus of elasticity.	Work to elastic limit. Height of drop caus-	Fiber stress at elastic	limit, Maximum erushing	strength. Modulus of elasticity.	Compression perpendic	fiber stress at class	Radial surface.	Tangential surface.	Surface of failure radial,	Surface of failure tangential.	erulist to sostrug	Surface of failure tangential.	eurlase to sestrug	Surface of failure fangential.
		1	Per cent.	P B B	Per cent of di- mensions when green.		Lbs. per sq. in.	L bs. per sq. in,	1,000s of lbs.	fnch lbs.	Inch lbs. per cu.in. Inch lbs.	per cu. in.	for sold and a sold and a sold and a sold a	per sq. in.	,ni .uo 19q	Inches.	sq.in.	aq.in.	per sq. in.	sq.in.	Lbs.	L.bs.	Lbs. per	Lbs. per	Lbs.	Lbs.	Lbs. per	req sd.I
III.—ACTUAL VALUE OF	VALU	E OF	1	GH P	EACH PROPERTY FOR EACH	GRTY	FOF	3 EA		SPE	CIES	LOC.	ALIT		"SPECIES-LOCALITY" AS DETERMINED BY EQUATION VALUE—Continued.	ETE!	MIN	ED	8Y T	EST	S-E	CPR	TESTS-EXPRESSED IN PERCENTAGE	NI O	PER	CEN	LAG!	3 OF
1	- 8	69	Ą	10	9	t-	00	01	10	===	12	51	41	15	191	17 1	18 19	9 20	21	122	- 23	- 24	52	36	72	8	8	30
CONTERS—Contd. Fir, grand (Mon-	2																	-										
Green	88		-:	101	88	107	110	800	138	<u>7</u> 8	15.24	120	120	128	127	139 13	128	101	168 100		106 95 113 98	104	111	200	328	88	84	22
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Fir, white (C.	<u> </u>	-	<u>:</u>	<u>:</u>			<del>:</del>	•		$\dot{}$	<del>: -</del>	:	<u>:</u>	:	:	<u>:</u>	-	<u>:</u>	<u>:</u>	<u>:</u>	<u>:</u>	<u>:                                    </u>	<u>:</u>	<u>:</u>	<u>!</u>	<u>!</u>	<u>!</u>	<u> </u>
Green				8	201	871	136	116	ă	691	<b>a</b>	83	111	128	E E	100	144	116	132 146		106	90	118	99	2	1	<b>ಹ</b> [	85
Afrdry	:	-:	_		<u> </u>	:	_	_		137	_	_	_	_	_	_	_		_	_	_	_	_		_	_	•	3

101 88	28.82	118		45		<b>\$</b>	8	8	28		2	
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558	121	118		8		88	5	8	8.	88	8	
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135	133 149	164		8		2	101		88	130	95	
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100	108	84	<u>:</u>	88		2	26	107	. 8	113	108	
011.	<b>Z</b>	2		88		<b>50</b>	8.	421	114	119	130	
8	35	8		83		2	8.	8	28	91	115	
			_::									
4	23	15	26	22	2	127	3	8		æ	356	
Hemlock, black (Montana): Green Air-dry Hemlock	(Tennessee): Green Air-dry	(Wisconsin): (Green. Alr-dry. Hemlock, western	(Washington); Green. Air-dry	(Montana): Green.	Larch, western (Washington): Green.	Pine, Cuban (Floridae)	Pine, jack (Wisconsin) Sin): Green	Pine, Jeffrey (California): Great	Pine, loblolly (Florida): Ida): Green	Pine, lodgepole (Colorado): Green. Air-drv	1в Зу,	

Table 1.—Equations and variations—specific gravity, shrinkage, and strength relations based on tests of small clear pieces, green and air-dry—Con.

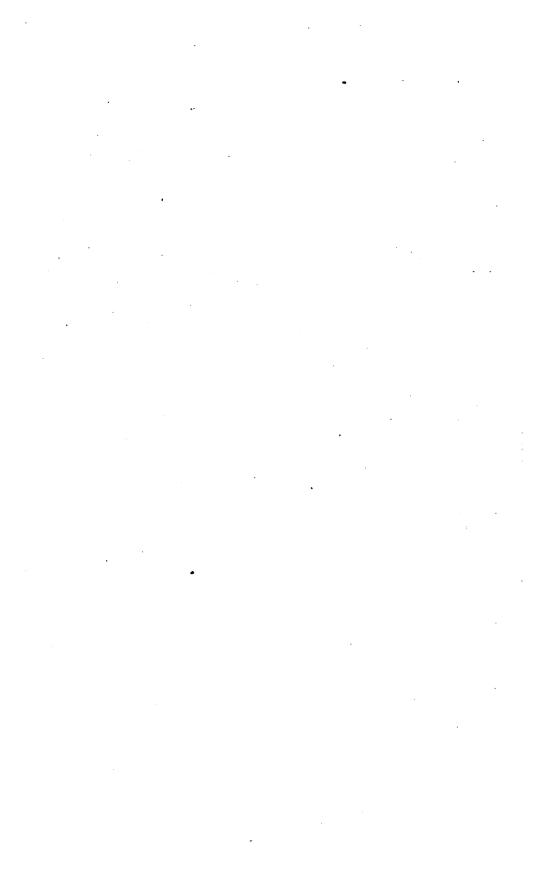
sion.	Surface of failure tangential.	Lbs. per	E OF	30	89	65
Ten	eurlist to eastrug	Lbs. per sq. in.	[AG]	29	89	72
Cleavage. Tension.	Surface of failure tangential.	Lbs.	CENT	82	29	99
Cles	Surface to failure fails.	Lbs.	PERCENTAGE	27	92	29
ar.	Surface of failure tangential.	Lbs. per sq. in.	Ä	56	52	8
Shear.	Surface to searing salure laiber	Lbs. per sq. in.	TESTS-EXPRESSED	13	8	8
red a ball ts	Tangential surface.	Lbs.	RES	24	\$8	8
Hardness: load required to embed a 0.444-inch bal one-half its diameter.	Radial surface.	Lbs.	EXP	23	. 28	92
Had 10ad 4.4. of the digital distribution of the digital distribution of the distribut	End surface.	Lbs.	TS	22	47	72
cular to grain, stic limit.	Compression perpendic	Lbs. per sq. in.	TES	21	67	4
	Modulus of elasticity.	1,000s of lbs. per sq. in.	BY	20	041	165
Compression parallel to grain.	Maximum crushing strength.	Lbs. per	EACH "SPECIES-LOCALITY" AS DETERMINED BY EQUATION VALUE—Continued.	19	96	103
Com para g	Fiber stress at elastic limit.	Lbs. per	3RM1	81	86	88
eg.	Height of drop caus- ing complete failure.	Inches.	DETI ued.	17	. 101	33
Impact bending, 50-pound hammer	Work to elastic limit.	Inch lbs. per cu. in.	AS Jontin	16	102	8.
act b und l	Modulus of elasticity.	1,000s of lbs. per sq. in.	ξξ Ε	15	112	112
Imi 50-po	Fiber stress at elastic limit.	Lbs. per sq. in.	ALU	11	100	16
	Total work.	Inch lbs.	NC NC	13	98	98
	Work to maximum load.	Inch lbs. per cu. in.	CIES	12	. 18	88
ndiba	Work to elastic limit.	Inch lbs. per cu. in.	SPE EQU	=	8	28
Static bending	Modulus of elasticity.	1,000s of lbs. per sq. in.	, но	2	105	112
Sta	Modulus of rupture.	l.bs. per	S EA	6	98	8.
	Fiber stress at elastic limit.	Lbs. per sq. in.	FOR	36	54	26
6 6 - 10 i	Tangential.		RTY	14	86	105
Shrinkago from green to oven- iry condition.	Radial.	Per cent of di- nensions when green.	PROPERTY	9	83	122
Shrinkago from green to oven- dry condition.	In volume.	Per cent of di- mensions when green.		7.0	105	105
	Moisture content.	Per cent.	<b>ACE</b>	4		: :
-dry, based on of test,	Specific gravity, oven-		OF E.	m		
<del>`</del>	Reference number.		3 D.	61	418	40a
	Species and locality.		II.—ACTUAL VALUE OF	1	COMPERS—CONTG.  Pine, 1 odge p ole (Granite County, Montana).  Area.	le ty,

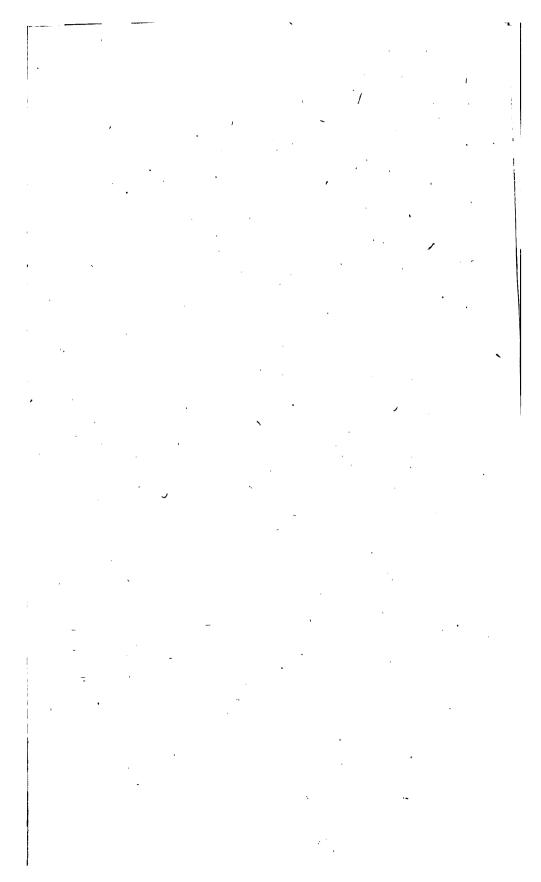
	36	<b>.</b> 4	25 25	4	48	1001	88		100	13 :	34
	34	<u> </u>	42	45	<del>\$</del> 17	82	51		<u>z, 8</u>	29	8
114	88	#	8.4	45	678	23	88		011	82	<u>\$2.53</u>
858	. 8	\$	128	器	8.73	88	\$		112	22	8:8
688	23	₩	88	88	78	<b>88</b>	79	38		88	<u>\$</u>
86	88	8	8.E	\$	88	83.2	8	83	126	88	46
81	2	8	\$8	22	2,8	<b>88</b>	23		102	81	88
81	19	67	38	8	25.22	% <b>2</b>	23		2,8	22	28.8
258	20	18	86.7	33	38.82	82	88		96 110	88	47
106	8	8	88	92	13	88	8	13	121	88	110
28	Ħ	22	125	112	<u> </u>	88 89	26		100	882	141
2, 2,	110	118	117	111	523	26.22	105	88	105	102 102	113
88.83	113	127	211	120	102	88	105	133	22 25	901	131
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10.5	<b>8</b>	8	12.88	4	22 106	138	88		119	121	82
88	8	Ξ	901 011	168	107 115	96	100		01 101	104 110	118
28	25	16	8.2	16	88	<u>\$</u> 5	83		25	182	. 851
84	8	7.	<u>\$</u> 2	8	21 110 110	114	<b>.</b>		82	102 17	117
88	22	8	88	19	88	82	88		88	28	74
87 154	84	8	8.2	100	88	88	102	95	140 139	110	24
<u>58</u>	. 21	11	128	107	ឌ្ឌឌ	83	101	117	901	¥01 100	132
85	8	8	<u>\$</u>	\$	95	88 78	26	105	901	88	88
88 110 80	10	115	859	8	86 119	88	102	107	113	107	921
22	7	88	8		8	8	88		ર્જ	18	11
<u> </u>	88	<u>§</u>	119	8	8	107	101		8	Ŗ	109
8	7.	88	*	7.	8	84	4		88	62	10g
*	8	<u> </u>	8	95	52	5	88	#.	ន	88	ដ
Pine, lodgepole (Wyoming): Green Air-dry	ida): Green	Pine, longlesi (Lake Charles, Louisi- ana): Green	Pine, longleaf (Tangipahoa Parish, Louisiana): Green Air-dry	Pine, longleaf (Mississippi): Green	Pine, Norway (Wis- consin): Green Air-dry Pine, pitch (Tennes-	see): Green Air-dry Pine, pond (Flori-	da): Green Air-dre	Pine, shortleaf (Ar- kansas): Green Air-dry	Pine, sugar (California): Green Air-dry	Air (Tennessee): Green Air-dry Pina western white	(Montana): Green Air-dry

TABLE 1.—Equations and variations—specific gravity, shrinkage, and strength relations based on tests of small clear pieces, green and air-dry—Con.

ďo ť	Surface of failure tangential.	Lbs. per	Ö	8		114	141	£ 3	1 ;
Tension	Surface of failure fadial.	Lbs. per	AGE	68		121	142	88	•
	Surface of failure tangential.	Lbs.	TESTS-EXPRESSED IN PERCENTAGE	88		114	98	101	
Clesvage.	Surface of failure radial.	Lba.	ERC	27		112	<u> </u>	92	₹5
	Surface of failure tangential.	Lbs. per	Zi.	28	İ	9	<u> </u>	88	<b>28</b> 8
Shear.	Surface of failure radial,	Lbs. per sq. in.	SED	83		103		88	88
s: red la ball ts	Tangential surface.	L.ba.	RES	77		88	 8	<b>88</b> 8	228
Hardness: load required to embed a 144-inch ball one-half its diameter.	Radial surface.	Lbs.	EX	23		35	112	23	883
108d 108d 0.444 0.444 dig	End surface.	L.be.	STS	52		92	 8	82	. 58
ular to grain, tic limit.	Compression perpendio	Lbs. per sq.in.		12		8	114	18	6119
	Modulus of elasticity.	1,000s of lbs.	) BY	82		8	8	118	55.
Compression parallel to grain.	Maximum crushing strength.	Lbs. per sq. in.	INE	2		16	011	85	162
Com	Fiber stress at elastic limit.	Lbs. per sq.in.	"SPECIES-LOCALITY" AS DETERMINED EQUATION VALUE—Continued.	18		133	91	105	101
ig,	Height of drop caus- ing complete failure.	Inches.	DET.	11		81	2	55	<b>8</b> 8
Impact bending, 59-pound hammer.	Work to elastic limit.	per cu. in.	AS	16		116	à	112	8.8
ound	Modulus of elasticity.	1,000s of lbs.	TY."	15		35	3	882	88
F. 149	Fiber stress at elastic limit.	Lbs. per sq. in.	CALI	14		26	\$	88	25
	Total work,	Inch lbs. per cu. in.	S-LO ON	13		8	<u> </u>	25	E E
ò	Work to maximum load.	per cu. in.	CIE	12		88	3	22	88
Static bending.	Work to elastic limit.	Inch lbs. per cu. in.	"8P)	n		8	135	28.5	<b>5</b> 9
atte b	Modulus of elasticity.	1,000s of lbs. per sq. in.		10		25	<del>2</del> 2	113	₹8
22	Modulus of rupture,	Lbs. per sq.in.	PROPERTY FOR EACH	6		8	\$	88	8:
	Fiber stress at elastic limit,	Lbs. per sq.in.	F.0	00		8	Ę	88	88
from ven- tion.	Tangential.	of di-	SRTS	4		107		#	. 82
Shrinkage from green to oven- dry condition.	Radial	Per cent of di- mensions when green.	ROFI	9		122	-	22	25
Shrir greet dry	In volume,	Permens		23		16		88	8.
	Moisture content.	Per cent.	EACH	4					
dry, based on of test.	Specific gravity, oversemit as emuloy		<b>4</b> 0	60		- 5		:	
	Reference number.		LUE	CH		19		37	#
	Species and locality.		III.—ACTUAL VALUE	1	CONTERS—contd.	Pine, western yellow (Arizona):	Pine, western (Cell- formia):	Green	Pine, western (Colo- rado): Green Air-dry

101	85 97	; ;	;;	::		::	8.8	Ħ	99 :	63	45
261	28.28						125	83	29	79	2
88	87			2,8	88	% 20 €	190	88	82	52	84
252	882			881	201	82	88	82	88	81	\$4
88	<u>%</u> 2	£5	28	82	82	82	97	891	6	829	122
95	88	62	8	86	75	252	88	108	<u>0</u>	88	135
101	88			90	99	183	103	88	2	88	911
88	86 115			858	10g 10g	88	88	28	æ	72	119
82	109			100	82	88.22	114	916	8	88	115
111	108	118	88	137	142	18	611	100	8	88	240
100	128	85	115	110	113		127	133	2	114	82
88	108	165	124	97	87	107	201	88	8	108	102
105	124	143	103	113	95.8		152	129	411	108	325
801	<b>8</b> 2			85 116	88	144	æ31	139	ō.	82	8 :
139	85			126	104	100	112	105	22	<b>4</b> 88	82.83
11.88	108			88	82	109	120	115	8	928	288
288	28			88	38	8.	105	88	26	88	86
110	172			114	88	149	118	88	8	96	126
	101			107	888	88	252	139	82	17.22	88
121	158			130	2128	116	20.05	146	136	512	821
89	123 123 134	88	22.2	100	929	117	88	113	22	100	38
88	58	101	113	117	88	222	20.20	124	88	228	228
113	122	88	252	107	<b>%</b>	108	92 128 128	82128	100	97	84
22	8.			125	121		126		115	8	23
8	2			121	107		100		28	29	8
- 24	1			117	83		115		4	101	22
33	8	88	<b>B</b>	80	w 4		8	7	88	25	134
tana): Green	consin): Green Air-dry Redwood (Albion,	California): Green Air-dry Redwood (Korbel,	Guidornia): Green Air-dry Spruce, Engelmann	Colorado): Green Air-dry Spruce, Engelmann (San Miguel Coun-	ty, Colorado): Green Air-dry Spruce, red (New	Hampshire): Green Air-dry Spruce, red (Ten-	nessee): Green Air-dry Spruce, white (New	Hampshire): Green Air-dry Spruce, white (Wis-	Consin): Green Air-dry	sin): Green. Air-dry. Yew, western	
Pine tar	Red	5 P	5 7 E		ty {Spruge	<b>第一点</b>	a Z	Spruge		Sin): Gray	€~





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